

Rx antennas at IV3PRK: the Waller Flag

Upgrading from the rotatable Flag by W7IUV, and its original K6SE design, to the “Waller Flag”, an end-fire rotatable two loops array by NX4D and N4IS.

Rotatable Flag interactions with the Tx antenna.

My transmitting antenna is a top loaded, shunt-fed tower with four elevated $\frac{1}{4}$ wave radials, at a distance of 28 meters from the rotatable Flag. I included it into the Eznec model and rotated the Flag wires in 30 degrees increments to see which were the effects of the nearby Tx antenna. As expected, and as it is in the reality, the RDF and specially the FB deteriorate very much when the Flag is facing the Tx antenna; on some bearings, the pattern is totally destroyed.

In the following plots we see the difference between the patterns of the Flag alone (primary black trace), and when adding the Tx tower in that direction (red trace).

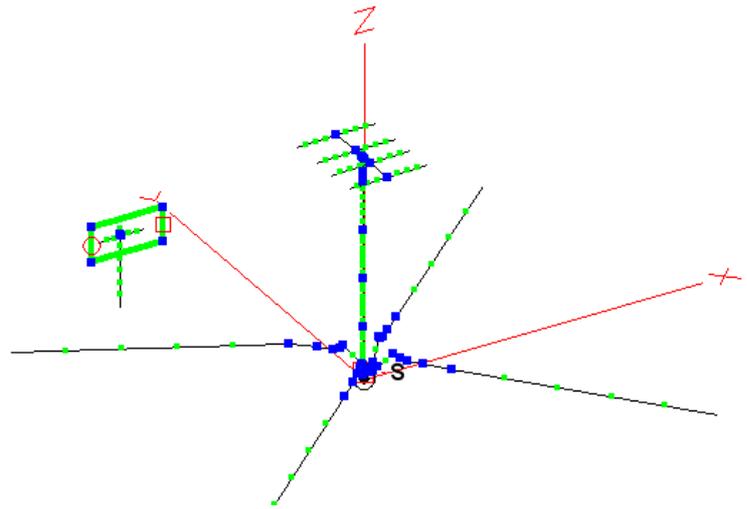


Fig.1: Eznec “View antenna” snapshot

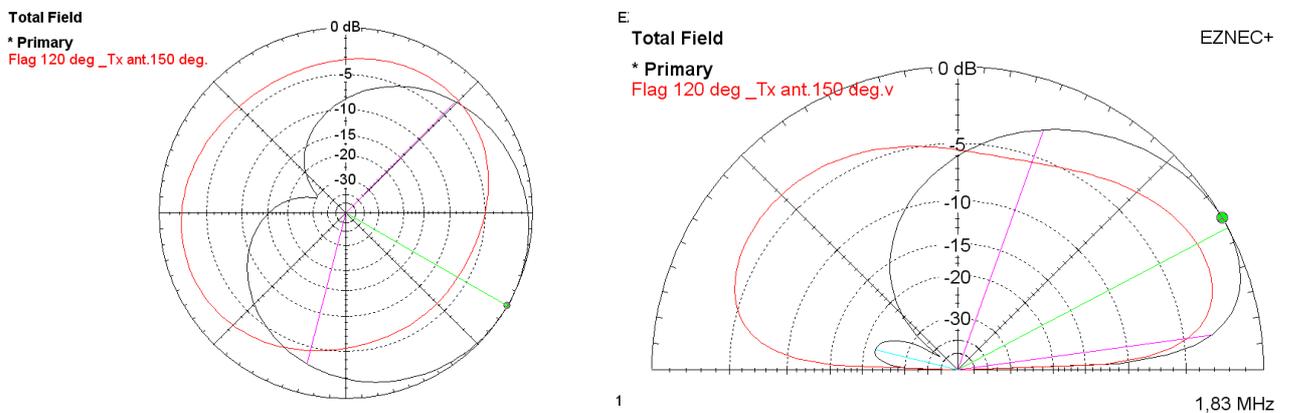


Fig.2: Azimuth and Elevation pattern deterioration of the Flag when facing the Tx antenna

In order to see the Tx antenna detuning effect, I added, in the Eznec model, a $\frac{1}{4}$ wavelength shorted stub (a high impedance) at the base of the tower. The offending vertical obstruction, (offending during reception, of course), disappears and I summarized the behaviour of the two highlights in the following Excel graphs.

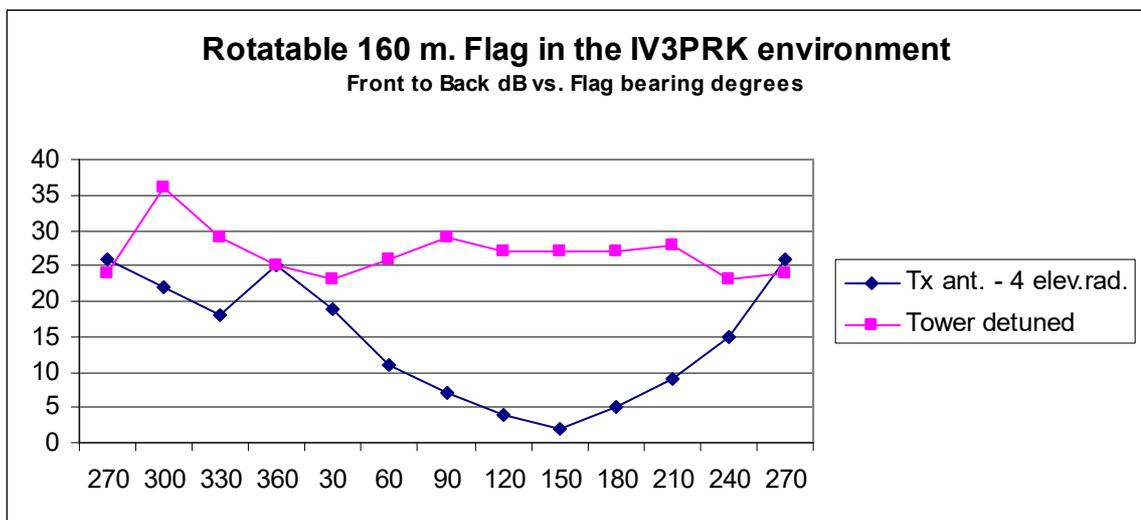
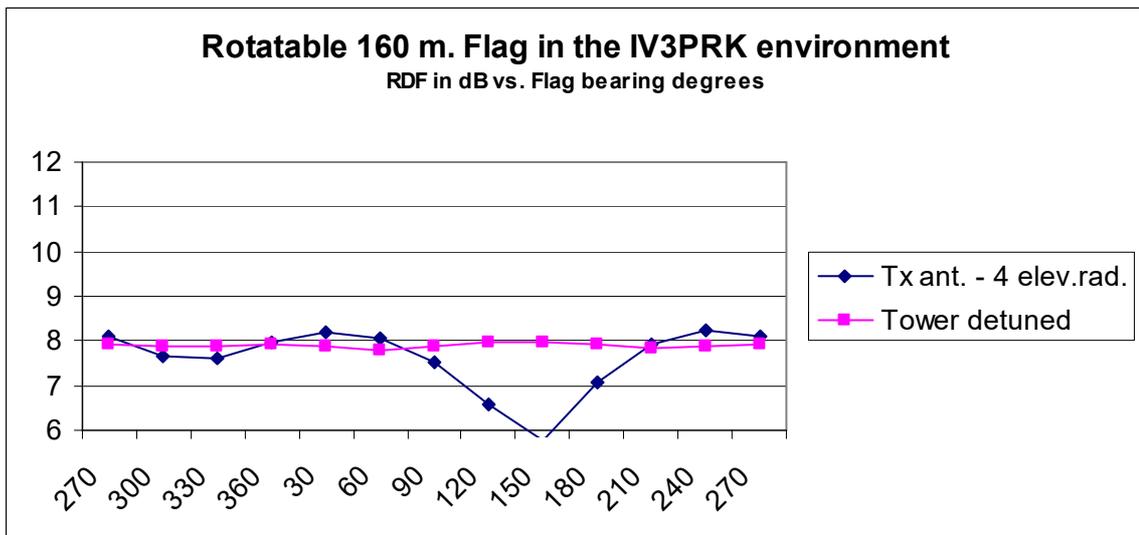


Fig.3 and 4: Rotating with Eznec the W7IUUV Flag before and after detuning the Tx antenna

While the RDF remains fairly flat, ranging from 7.81 to 7.96, the Front to Back still shows some minor variations due to the elevated radials; a strange positive effect is given at 300 degrees bearing by the radial in that direction and beneath the Flag.

Of course, detuning the “real” Tx antenna is not that easy as with the Eznec model: connecting and switching a 90 degrees coax cable at the feedpoint does not work. It’s a must now to learn the method used by Tom, W8JI or Carlos, N4IS, and climb the tower for the mechanical work.

[The Waller Flag](#)

After hearing directly how well Jose Carlos N4IS was working DX stations on 160 m. from southern Florida, also in the spring/summer season, and knowing the success achieved in a few years by Doug NX4D himself, I was attracted by their receiving antenna.

It is a rotatable end-fire close array of two Flags, originated by Doug Waller NX4D and thus named “The Waller Flag” by Jose Carlos N4IS, who built a couple of them with improvements.

All the electrical and mechanical details are on his web page www.n4is.com : with over 11.5 dB of RDF, it can be compared to a rotatable broadside array of two 175 m. Beverages. But, as usual, there is no free lunch with antennas and its drawback is a very low signal level, around “ - 55 dB”, which is about 40 dB lower than the Beverages. Hence, not only one, but two good preamplifiers are needed and be very careful against common noise entering the coax cable.

Modeling with EZNEC.

I wanted to upgrade my rotatable W7IUV Flag into the new Waller Flag and thus the starting point and constraints were the physical dimensions of the boom and the fiberglass spreaders. First step was to choose the phasing line lengths to the two loops and these results are summarized in the following table.

Table 1: The Waller Flag - Starting model - Transmission Lines SWEEP

File	TL1 mt.	TL2 mt.	gain	TO angle	Bearing	BW	FB	Avg.gain	RDF
N4Flag_0	4,00	3,00	- 58,02	20	267	68	15	- 69,86	11,84
wires 8 - segm. 120	4,00	3,25	- 57,49	20	267	70	16	- 69,37	11,88
WF alone: 12 m.length , 12 m.high	4,00	3,50	- 56,99	20	267	71	17	- 68,86	11,87
2 loops (4,27 x 2,00 m.) 5 m. sep.	4,00	3,75	- 56,53	20	267	76	18	- 68,34	11,81
Xfmr: 600/100 ohms	4,00	4,00	- 56,08	23	269	74	19	- 67,82	11,74
Load resistor RL1= 600 ohm	4,00	4,25	- 55,65	23	267	75	20	- 67,30	11,65
Load resistor RL2= 600 ohm	4,00	4,50	- 55,24	23	267	81	20	- 66,80	11,56
Transm. line: 100 ohm (2 x RG58)	4,00	4,75	- 54,85	23	267	82	21	- 66,31	11,46
TL1 to front loop	4,00	5,00	- 54,48	23	267	82	22	- 65,84	11,36
TL2 to rear loop reversed phase	4,00	5,25	- 54,13	23	267	83	23	- 65,39	11,26
	4,00	5,50	- 53,79	23	267	84	24	- 64,95	11,16
	4,00	5,75	- 53,47	23	267	86	25	- 64,53	11,06
	4,00	6,00	- 53,16	23	267	87	25	- 64,12	10,96
	4,00	6,25	- 52,86	23	267	88	26	- 63,73	10,87
	4,00	6,50	- 52,57	23	267	88	27	- 63,35	10,78
	4,00	6,75	- 52,29	23	267	89	28	- 62,99	10,70
	4,00	7,00	- 52,02	23	267	90	29	- 62,64	10,62
	4,00	7,25	- 51,76	23	267	93	30	- 62,31	10,55
	4,00	7,50	- 51,51	23	267	95	31	- 61,98	10,47
	4,00	7,75	- 51,27	23	267	96	32	- 61,67	10,40
	4,00	8,00	- 51,03	23	267	96	33	- 61,36	10,33
	4,00	8,50	- 50,58	23	267	97	36	- 60,79	10,21
	4,00	9,00	- 50,15	23	267	98	38	- 60,25	10,10
	4,00	10,00	- 49,37	23	267	101	36	- 59,26	9,89

My preferred area is the green shadowed, with the choice for TL1=4,00 m. and TL2=4,25 m. It's a compromise between maximum RDF - but with a high angle secondary lobe, (red line and red pattern below) and higher Front to Back - but with a broader lobe and a decreasing RDF (blue line and blue pattern).

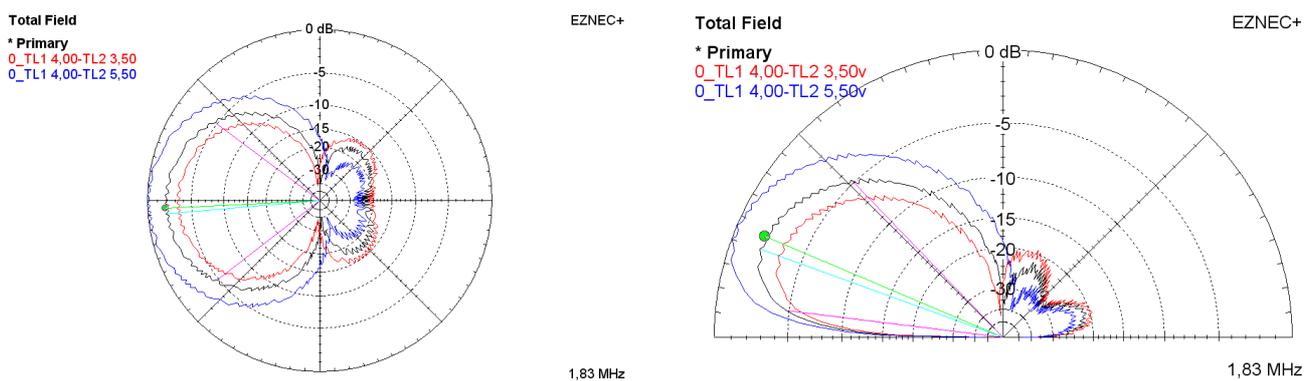


Fig.5: The Waller Flag alone in the air as from Table 1: primary pattern is for TL1 = 4,00 m. and TL2 = 4,25

In any case the phasing lines are NOT critical, as Table 2 shows the same results for one meter longer lengths on both sides.

Table 2 - The Waller Flag - Starting model - Transmission Lines SWEEP

File	TL1 mt.	TL2 mt.	gain	TO angle	Bearing	BW	FB	Avg.gain	RDF
N4Flag_0	5,00	2,00	- 63,08	26	153	56	9	- 70,72	7,64
wires 8 - segm. 120	5,00	2,50	- 62,01	19	269	54	9	- 71,19	9,18
WF alone: 12 m.length , 12 m.high	5,00	2,75	- 61,20	19	269	68	10	- 71,24	10,04
2 loops (4,27 x 2,00 m.) 5 m. sep.	5,00	3,00	- 60,45	19	269	60	11	- 71,17	10,72
Xfmr: 600/100 ohms	5,00	3,25	- 59,77	19	269	60	12	- 70,97	11,20
Load resistor RL1= 600 ohm	5,00	3,50	- 59,14	19	269	65	13	- 70,67	11,53
Load resistor RL2= 600 ohm	5,00	3,75	- 58,55	19	269	66	14	- 70,28	11,73
Transm. line: 100 ohm (2 x RG58)	5,00	4,00	- 57,99	20	267	68	15	- 69,84	11,85
TL1 to front loop	5,00	4,25	- 57,47	20	267	70	16	- 69,35	11,88
TL2 to rear loop reversed phase	5,00	4,50	- 56,98	20	267	71	17	- 68,85	11,87
	5,00	4,75	- 56,52	20	267	76	17	- 68,33	11,81
	5,00	5,00	- 56,08	23	267	74	19	- 67,82	11,74
	5,00	5,25	- 55,65	23	267	75	20	- 67,31	11,66
	5,00	5,50	- 55,25	23	267	81	20	- 66,82	11,57
	5,00	5,75	- 54,87	23	267	82	21	- 66,33	11,46
	5,00	6,00	- 54,50	23	267	82	22	- 65,87	11,37
	5,00	6,25	- 54,15	23	267	83	23	- 65,42	11,27
	5,00	6,50	- 53,82	23	267	84	24	- 64,98	11,16
	5,00	6,75	- 53,50	23	267	86	24	- 64,56	11,06
16ft - 23ft NX4D design ==>	5,00	7,00	- 53,19	23	267	87	25	- 64,16	10,97
	5,00	7,25	- 52,89	23	267	88	26	- 63,77	10,88
	5,00	7,50	- 52,60	23	267	88	27	- 63,40	10,80
	5,00	7,75	- 52,33	23	267	88	29	- 63,04	10,71
	5,00	8,00	- 52,06	23	267	90	29	- 62,69	10,63
	5,00	8,50	- 51,55	23	267	95	31	- 62,03	10,48
	5,00	9,00	- 51,07	23	267	96	33	- 61,42	10,35
	5,00	10,00	- 50,19	23	267	98	38	- 60,30	10,11

Impedance matching.

A very useful feature of the new EZNEC 5 version is the possibility to add to the model transformers and other impedance matching objects, and to analyze the antenna system as a whole.

Thus, I placed where they have to be, two Xfmrs designed to transform the loop impedance of 600 ohms (Z_p) to characteristic impedance of 100 ohms (Z_s) of the phasing lines made up with two RG58 cables in parallel. At the "T" junction, where one of the lines is reversed, we find 50 ohms with a satisfactory SWR of 1:1,2.

To calculate the real transformer I used the following procedure:

1. The reactance of the windings should be at least four times the impedance the winding is designed to look into.

So, $600 \times 4 = 2400$ ohms of reactance for the primary. Using 1.8 MHz as the lowest frequency, the inductance would need to be: $L = 2400 / 2 \times \mu \times 1.8\text{MHz}$.

So: $2400 / (6.28 \times 1.8) = 212$ microhenry

2. To find the number of turns the formula is: $N = 1000 (\text{SQRT} (L \text{ in mH} / AL))$

I have two ferrite cores available: the FT114-77 toroids with $AL = 1140$, and the preferred binoculars BN73-202 with $AL = 8500$.

So, $N = 1000 (\text{SQRT} (0.212 / 1140)) = 13.65$ turns on the primary for the FT114-77

Or, $N = 1000 (\text{SQRT} (0.212 / 8500)) = 5.00$ turns on the primary for the BN73-202.

3. To find the number of turns on the secondary the formula is: $N_p / N_s = \text{SQRT} (Z_p / Z_s)$,

So: $N_p / N_s = \text{SQRT} (600/100) = 2.45$, which is the ratio of the primary to secondary turns.

Thus, $N_s = 13.65 / 2.45 = 5.57$ turns on the secondary of the FT114-77 core

Or, $N_s = 5.00 / 2.45 = 2.04$ turns on the secondary of the BN73-202, much better.

It is easier to wind a small binocular core with only five and two turns and that's definitely my choice, according also to the W8JI advice on the 73 material.

Twinking the model for best Front to Back.

The following table summarizes many runs at the search of the load resistor values which give the highest Front to Back ratio, provided the desirable RDF already reached.

It is confirmed, once again, that the Waller Flag “wants to work” in every case, but the green shadowed areas are better and for sure, with this model (clear in the air without any supporting structure), the best combination is found with 500 ohms on the front loop and 520 on the rear one.

In the last two columns we see the impedance, always with an acceptable SWR, found on the feeding point, which is at the 100-ohm phasing lines junction.

Table 3: The Waller Flag - Starting model - LOAD Resistors SWEEP

File	RL1	RL2	gain	TO ang.	BW	FB	Avg.gain	RDF	Imped. R.	Imped. jX
N4Flag_0	350	400	- 58,39	19	66	10	69,09	10,70		
wires 8 - segm. 120	375	400	- 57,11	23	70	15	68,77	11,66		
WF alone: 12 m.length , 12 m.high	385	400	- 56,66	23	73	17	68,41	11,75	40,3	21,0
2 loops (4,27 x 2,00 m.) 5 m. sep.	390	400	- 56,44	23	73	17	68,21	11,77		
Xfmr: 600/100 ohms	395	400	- 56,24	23	73	17	67,98	11,74		
Load resistor RL1 on front loop	400	400	- 56,04	23	74	17	67,75	11,71		
Load resistor RL2 on rear loop	450	500	- 57,84	19	68	17	69,26	11,42		
Transm. line: 100 ohm (2 x RG58)	475	500	- 56,91	20	73	31	68,74	11,83		
TL1 to front loop = 4,00 m.	480	500	- 56,74	23	73	32	68,59	11,85	48,4	14,8
TL2 to rear loop rev.phase = 4,00 m.	485	500	- 56,58	23	73	30	68,42	11,84		
	490	500	- 56,41	23	74	26	68,24	11,83		
	495	500	- 56,26	23	74	24	68,06	11,80		
	500	500	- 56,10	23	74	22	67,87	11,77	49,2	14,2
	500	515	- 56,56	23	74	31	68,41	11,85		
	500	520	- 56,71	23	73	38	68,56	11,85	49,9	13,5
	500	525	- 56,86	20	73	33	68,70	11,84	50,0	13,4
	505	525	- 56,71	23	73	37	68,55	11,84		
	500	550	- 57,61	19	69	19	69,18	11,57	51,0	12,7
	530	550	- 56,66	20	75	26	68,51	11,85	52,0	11,0
	550	600	- 57,39	20	70	18	69,03	11,64	54,4	9,3
	555	600	- 57,25	20	71	19	68,95	11,70		
	560	600	- 57,11	20	71	20	68,86	11,75		
	565	600	- 56,97	20	73	21	68,76	11,79		
	570	600	- 56,83	20	75	21	68,64	11,81		
	575	600	- 56,70	20	75	21	68,52	11,82		
	580	600	- 56,57	20	76	21	68,39	11,82	55,4	8,2
	585	600	- 56,44	20	76	20	68,26	11,82		
	590	600	- 56,32	20	76	19	68,11	11,79		
	595	600	- 56,20	23	74	19	67,97	11,77		
	600	600	- 56,08	23	74	19	67,82	11,74	56,8	7,0
	605	600	- 55,96	23	75	18	67,66	11,70		
	610	600	- 55,85	23	75	17	67,51	11,66		
	615	600	- 55,73	23	75	17	67,35	11,62		
	620	600	- 55,62	23	75	16	67,20	11,58		
	625	600	- 55,51	23	75	16	67,04	11,53	56,8	6,7
	630	600	- 55,41	23	81	15	66,88	11,47		
	635	600	- 55,30	23	81	15	66,72	11,42		
	640	600	- 55,20	23	81	14	66,56	11,36		
	650	600	- 55,00	23	81	13	66,25	11,25		
	650	700	- 57,02	20	73	15	68,66	11,64	60,4	2,0
	670	700	- 56,58	20	76	15	68,32	11,74		
	675	700	- 56,48	20	76	15	68,22	11,74		
	680	700	- 56,38	20	76	15	68,12	11,74		
	685	700	- 56,28	20	76	15	68,01	11,73		
	690	700	- 56,18	20	76	15	67,89	11,71		
	695	700	- 56,09	23	74	15	67,78	11,69		
	700	700	- 55,99	23	74	15	67,66	11,67		
	725	700	- 55,54	23	81	14	67,05	11,51		
	750	800	- 56,69	20	76	12	68,27	11,58		
	775	800	- 56,27	20	76	12	67,89	11,62		
	785	800	- 56,11	20	76	12	67,72	11,61		
	790	800	- 56,03	20	76	12	67,64	11,61		
	795	800	- 55,95	20	76	12	67,55	11,60		
	800	800	- 55,88	23	75	12	67,45	11,57	66,4	6,7
	850	900	- 56,41	20	76	10	67,88	11,47		
	875	900	- 56,07	20	76	11	67,57	11,50		
	880	900	- 56,00	20	76	11	67,50	11,50		
	885	900	- 55,94	20	76	11	67,43	11,49		
	890	900	- 55,87	20	76	11	67,36	11,49	69,8	13,5

So, keeping now the load resistors fixed, I swept again the phasing line lengths at the search of any possible further improvement. Increasing the length of TL2 produces a broader forward lobe, with a better FB, but reduces the RDF. Making TL2 shorter than TL1 produces a narrow forward lobe, with enhanced RDF, but also the rise of an undesirable high angle back lobe.

Table 4: The Waller Flag - Starting model - final TWEAKING on the TL lines

File	TL1 mt.	TL2 mt.	gain	TO angle	Bearing	BW	FB	Avg.gain	RDF
N4Flag_0	3,00	2,50	- 57,76	20	267	70	30	- 69,69	11,93
wires 8 - segm. 120	3,00	2,75	- 57,21	20	267	70	31	- 69,11	11,90
Only WF on 9 m.boom, 12 m.high	3,00	3,00	- 56,68	20	267	75	33	- 68,52	11,84
2 loops (4,27 x 2,00 m.) 5 m. sep.	3,00	3,25	- 56,18	23	267	74	42	- 67,93	11,75
Xfmr: 600/100 ohms	3,00	3,50	- 55,71	23	267	75	44	- 67,35	11,64
RL1= 500 - RL2 = 520	3,00	3,75	- 55,26	23	267	81	44	- 66,79	11,53
TL1 100 ohm to front loop	3,00	4,00	- 54,84	23	267	81	42	- 66,25	11,41
TL2 to rear loop 180 deg. phasing	3,00	4,25	- 54,45	23	267	82	40	- 65,64	11,19
	3,00	4,50	- 54,07	23	267	83	38	- 65,24	11,17
	4,00	3,00	- 58,97	19	269	65	26	- 70,70	11,73
	4,00	3,50	- 57,77	20	267	69	29	- 69,70	11,93
	4,00	3,75	- 57,22	20	267	70	31	- 69,14	11,92
	4,00	4,00	- 56,71	23	267	73	38	- 68,56	11,85
	4,00	4,25	- 56,23	23	267	74	41	- 67,99	11,76
	4,00	4,50	- 55,76	23	267	75	44	- 67,43	11,67
	4,00	4,75	- 55,33	23	267	78	44	- 66,88	11,55
	4,00	5,00	- 54,92	23	267	81	43	- 66,36	11,44
	4,00	5,25	- 54,53	23	267	82	41	- 65,85	11,32
	4,00	5,50	- 54,16	23	267	83	39	- 65,37	11,21
	5,00	4,00	- 58,92	19	269	65	26	- 70,67	11,75
	5,00	4,50	- 57,76	19	269	68	29	- 69,70	11,94
	5,00	4,75	- 57,23	20	267	70	31	- 69,15	11,92
	5,00	5,00	- 56,74	23	267	73	38	- 68,60	11,86
	5,00	5,25	- 56,26	23	267	74	41	- 68,04	11,78
	5,00	5,50	- 55,81	23	267	75	44	- 67,49	11,68
	5,00	5,75	- 55,39	23	267	78	45	- 66,96	11,57
	5,00	6,00	- 54,98	23	267	81	43	- 66,45	11,47
	5,00	6,25	- 54,60	23	267	82	41	- 65,95	11,35
	5,00	6,50	- 54,24	23	267	82	40	- 65,48	11,24
	5,00	7,00	- 53,56	23	267	84	37	- 64,59	11,03

The choice depends on local situations and personal needs. My priority is to keep as low as possible the high angle signals of European nearby stations, so I must stay in the black highlighted rows.

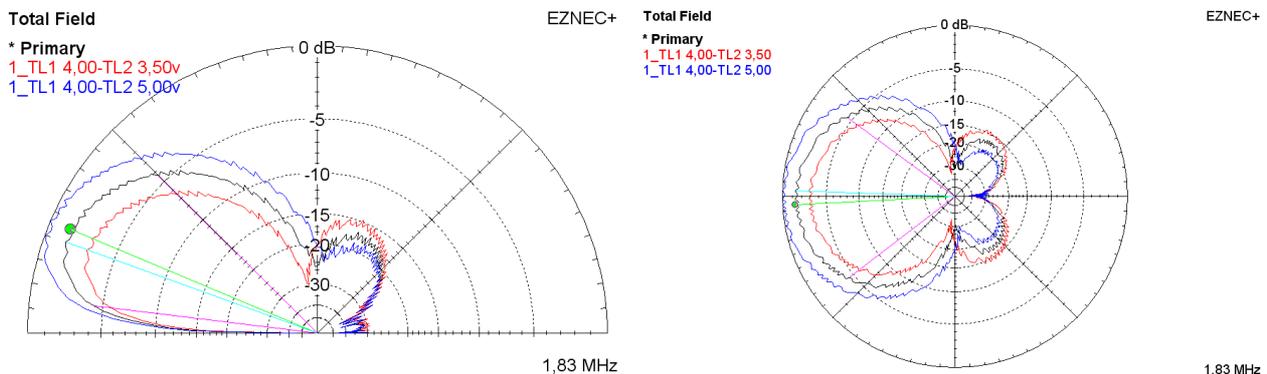


Fig.6: The Waller Flag alone in the air as from Table 4: primary pattern is for TL1 = 4,00 m. and TL2 = 4,25

Putting the Waller Flag model on its supporting tower and mast.

Now let's model the WF with its supporting tower and the boom/mast. No difference with a boom offset, like for the original Flag, so it's mechanically easier to put it directly on the mast.

Table 5: The Waller Flag - centered on its tower and boom/mast

File	gain	TO angle	Bearing	BW	FB	Avg.gain	RDF
N4Flag_01b	56,71	23	267	73	38	68,56	11,85
On the Air model							
wires 12 - segm. 135							
WF alone, 12 m.lenght, 12 m.high	270 - 55,88	20	272	77	21	67,38	11,50
2 loops (4,27 x 2,00 m.) 5 m. sep.	300 - 55,93	22	304	78	20	67,42	11,49
Xfmr: 600/100 ohms	330 - 55,85	20	330	78	22	67,37	11,52
RL1= 500 - RL2 = 520 ohms	360 - 55,92	22	0	78	20	67,43	11,51
TL1 100 ohm to front loop = 4 m.	30 - 55,94	22	30	79	21	67,44	11,50
TL2 to rear loop 180 deg. Rev. = 4 m.	60 - 55,89	22	60	79	21	67,40	11,51
	90 - 55,92	20	88	79	22	67,43	11,51
	120 - 55,89	22	122	80	21	67,38	11,49
	150 - 55,90	22	152	78	20	67,41	11,51
	180 - 55,83	20	180	78	21	67,39	11,56
	210 - 55,88	22	208	79	20	67,40	11,52
	240 - 55,87	22	232	78	21	67,32	11,45
	270 - 55,91	20	272	77	21	67,42	11,51

The added metal structure deteriorates the FB and the RDF parameters, so we have to tweak the model again.

Table 6: The Waller Flag - centered on its tower and boom/mast - now tweaking for best F/B

File	RL1	RL2	gain	TO angle	Bearing	BW	FB	Avg.gain	RDF
On the air model ==>	500	520	56,71	23	267	73	38	68,56	11,85
wires 12 - segm. 135									
WF alone, 12 m.lenght, 12 m.high	500	520	55,91	20	272	77	21	67,42	11,51
2 loops (4,27 x 2,00 m.) 5 m. sep.	550	600	56,56	20	272	76	19	68,01	11,45
Xfmr: 600/100 ohms	555	600	56,43	20	272	77	21	67,93	11,50
TL1 = 4m. TL2 = 4m.	560	600	56,30	20	272	77	23	67,84	11,54
TL1 100 ohm to front loop	565	600	56,18	20	272	77	25	67,75	11,57
TL2 to rear loop 180 deg. phasing	570	600	56,06	20	272	77	29	67,64	11,58
	575	600	55,94	20	272	77	32	67,53	11,59
	580	600	55,82	20	272	77	37	67,41	11,59
	585	600	55,71	20	272	77	37	67,29	11,58
	590	600	55,60	20	272	80	32	67,16	11,56
	595	600	55,49	20	272	80	29	67,03	11,54
	600	600	55,38	20	272	80	26	66,90	11,52
	600	605	55,49	20	272	80	28	67,04	11,55
	600	610	55,59	20	272	80	31	67,16	11,57
	600	615	55,70	20	272	78	34	67,28	11,58
	600	620	55,80	20	272	77	33	67,40	11,60
	600	625	55,90	20	272	77	30	67,51	11,61
	600	630	56,01	20	272	77	27	67,61	11,60
	600	640	56,21	20	272	77	23	67,79	11,58

The choice here is straightforward: increasing both load resistors by 80 ohms we recover the same F/B and about 0.10 dB in the RDF. Let's try again to improve also this last parameter.

Table 7: The Waller Flag - centered on its tower and boom/mast - last tweaking for best TL line lengths

File	TL1 mt.	TL2 mt.	gain	TO angle	Bearing	BW	FB	Avg.gain	RDF
FLFlag_02.EZ	5,50	4,00	58,74	20	272	67	28	70,45	11,71
wires 12 - segm. 135	5,25	4,00	58,19	20	272	70	30	70,00	11,81
WF 12 m.lenght, 12 m.high	5,00	4,00	57,67	20	272	72	32	69,51	11,84
2 loops (4,27 x 2,00 m.) 5 m. sep.	4,75	4,00	57,17	20	272	75	34	68,99	11,82
Xfmr: 600/100 ohms	4,50	4,00	56,70	20	272	76	36	68,47	11,77
RL1= 580; RL2 = 600 ohms	4,25	4,00	56,25	20	272	77	37	67,94	11,69
TL1 100 ohm to front loop	4,00	4,00	55,82	20	272	77	37	67,41	11,59
TL2 to rear loop 180 deg. phasing	4,00	4,25	55,42	20	272	80	37	66,91	11,49
	4,00	4,50	55,03	24	270	82	29	66,42	11,39
	4,00	4,75	54,66	24	270	82	29	65,94	11,28
	4,00	5,00	54,30	24	270	83	29	65,48	11,18
	4,00	5,25	53,95	24	270	85	28	65,04	11,09
	4,00	5,50	53,62	24	270	88	28	64,62	11,00

The RDF could be increased only on the side of TL1 lengthening, but with the undesirable rise of the high angle back lobe (red pattern). On the other side, stretching TL2, the RDF decreases further, with a broader beamwidth and a higher forward TO angle.

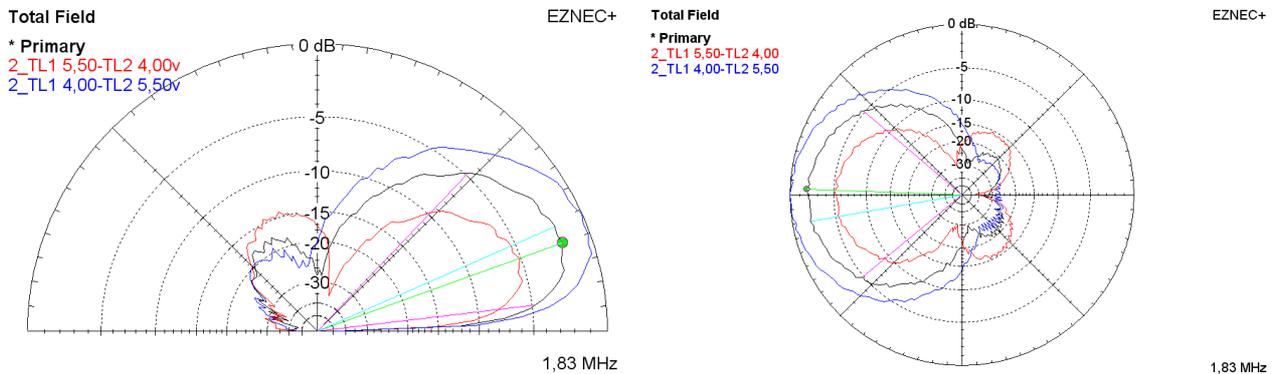


Fig.7: The Waller Flag on its tower as from Table 7: primary pattern is for TL1 = 4,00 m. and TL2 = 4,25

Interactions with the transmitting antenna.

Now let's add to the Eznec model all the wires forming the Tx tower, with its loading Yagi and the 4 elevated radials, as in Fig.1, and rotate the receiving antenna every 30 degrees.

More drastically than the standard Flag, due to its sharper lobe, the Waller Flag seems to be acceptable only when beaming on the opposite side of the Tx tower. Other than in West and North-West direction, the lobe is mostly destroyed.

Table 8: The Waller Flag - with its tower and boom/mast - plus the nearby Tx antenna and its 4 elevated radials									
File	gain	TO angle	Bearing	BW	FB	Avg.gain	RDF		
FLFlag_03	no interactions =>	- 55,42	20	272	80	37	- 66,91	11,49	
wires 67 - segm. 264	Beaming Degrees								
WF 12 m.l length, 12 m.high	270	- 56,77	20	272	74	15	- 68,38	11,61	
2 loops (4,27 x 2,00 m.) 5 m. sep.	300	- 54,22	22	304	86	19	- 65,30	11,08	
Xfmr: 600/100 ohms	330	- 53,73	20	330	89	17	- 64,49	10,76	
RL1= 580 - RL2 = 600	360	- 55,58	22	0	79	23	- 67,12	11,54	
TL1 100 ohm to front loop = 4,00 m.	30	- 58,43	20	22	78	8	- 68,60	10,17	
TL2 to rear loop 180 deg.rev = 4,25m.	60	- 58,32	20	62	83	7	- 68,21	9,89	
Added the wires of:	90	- 56,47	20	82	84	13	- 67,12	10,65	
Tx antenna at a distance of 38 m.	120	- 55,73	24	98	121	5	- 63,74	8,01	
and abt 140 degrees, with top loading	150	- 56,10	24	168	188	3	- 62,93	6,83	
yagi, 28 m. high, and 4 elev. radials	180	- 56,12	20	194	94	9	- 65,60	9,48	
	210	- 57,41	20	218	77	12	- 68,52	11,11	
	240	- 58,68	20	232	79	7	- 68,61	9,93	
	270	- 56,73	22	274	73	16	- 68,33	11,60	

But let's see what happens with Tx antenna detuning: just added in Eznec a high impedance, 90 degrees stub, on its feeding point.

Table 9: The Waller Flag - on its tower and boom/mast - plus the Tx antenna "DETUNED" and the same 4 elev.radials									
File	gain	TO angle	Bearing	BW	FB	Avg.gain	RDF		
FLFlag_03	no interactions =>	- 55,42	20	272	80	37	- 66,91	11,49	
wires 67 - segm. 264	Beaming Degrees								
WF 12 m.l length, 12 m.high	270	- 55,49	20	272	80	30	- 66,94	11,45	
2 loops (4,27 x 2,00 m.) 5 m. sep.	300	- 55,47	22	304	81	29	- 66,95	11,48	
Xfmr: 600/100 ohms	330	- 55,42	20	330	79	24	- 66,87	11,45	
RL1= 580 - RL2 = 600	360	- 55,50	20	4	81	23	- 66,89	11,39	
TL1 100 ohm to front loop = 4,00 m.	30	- 55,47	20	30	81	24	- 66,80	11,33	
TL2 to rear loop 180 deg.rev = 4,25m.	60	- 55,33	22	60	84	26	- 66,63	11,30	
Added the wires of:	90	- 55,41	20	88	82	23	- 66,88	11,47	
Tx antenna at a distance of 38 m.	120	- 55,69	22	122	81	25	- 67,26	11,57	
and abt 140 degrees, with top loading	150	- 55,80	22	152	81	22	- 67,25	11,45	
yagi, 28 m. high, and 4 elev. radials	180	- 55,51	20	180	79	26	- 66,97	11,46	
TL3 short ckt 90 degr. on Tx ant.	210	- 55,28	22	208	82	23	- 66,75	11,47	
	240	- 55,33	22	232	81	27	- 66,73	11,40	
	270	- 55,46	20	272	83	30	- 66,91	11,45	

Wow! The offending Tx antenna disappeared, and the Waller Flag recovered its behaviour and a clean pattern in every direction. A few dB are still missing in the FB, but this is not an issue.

Anyway, remember that the elevated radials were so detrimental on all my Pennants that every effort in tower detuning had no effect unless changing the ground system, so I modeled also this situation, to see if I could get any further improvement.

Table 10: The Waller Flag - on its tower - plus the Tx antenna "DETUNED" and a new "on ground" radial system

File	gain	TO angle	Bearing	BW	FB	Avg.gain	RDF
FLFlag_04	- 55,42	20	272	80	37	- 66,91	11,49
wires 166 - segm. 503	Beaming Degrees						
WF 12 m.l. length, 12 m.high	270 - 55,44	24	270	79	24	66,86	11,42
2 loops (4,27 x 2,00 m.) 5 m. sep.	300 - 55,56	22	304	80	29	67,06	11,50
Xfmr: 600/100 ohms	330 - 55,54	20	330	78	32	67,09	11,55
RL1= 580 - RL2 = 600	360 - 55,55	22	0	81	27	67,00	11,45
TL1 100 ohm to front loop = 4,00 m.	30 - 55,36	22	30	81	26	66,80	11,44
TL2 to rear loop 180 deg.rev = 4,25m.	60 - 55,19	22	60	82	34	66,66	11,47
Added the wires of:	90 - 55,38	20	88	80	28	66,87	11,49
Tx antenna at a distance of 38 m.	120 - 55,62	22	122	80	24	67,21	11,59
and abt 140 degrees, with top loading	150 - 55,65	22	148	79	23	67,29	11,64
yagi, 28 m. high, and 32 ground radials	180 - 55,37	20	180	79	28	66,93	11,56
TL3 short ckt 90 degr. on Tx ant.	210 - 55,15	22	208	82	32	66,61	11,46
	240 - 55,19	22	232	81	26	66,62	11,43
	270 - 55,44	20	270	79	24	66,86	11,42

Only a negligible improvement, not worth the hard work of laying down a serious ground system, at least as receiving is concerned. On the transmitting side, of course, the antenna efficiency would be surely improved but, as long as I can work every Dx station heard, I can keep my four elevated radials without disturbing or damaging the green lawn. (Since my retirement, gardening became my first activity).

The most meaningful data of tables 8, 9 and 10 are better shown with the two graphs here on the right. No doubt that detuning the Tx antenna is a "must", but radials placement has some random effect only on the front to back ratio.

The main parameter of the RDF - *Receiving Directivity Factor* - is mostly flat and unaffected by radial system, contrary to what happens with the Pennants, which are close and at the same high of the elevated radials.

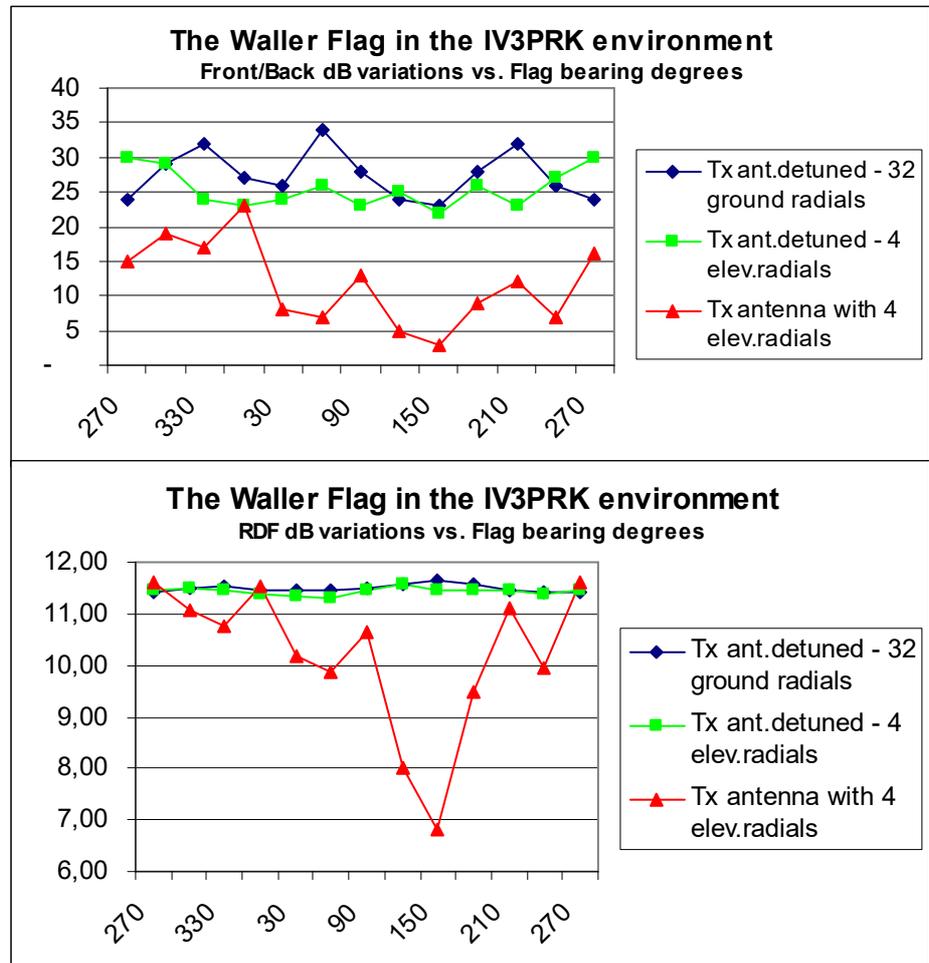
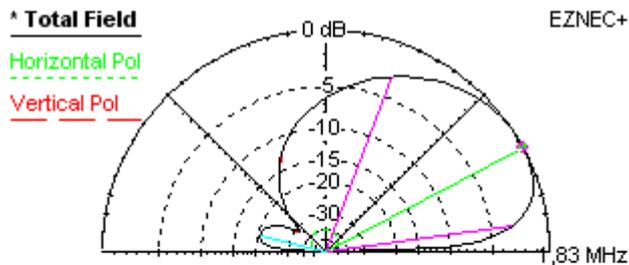


Fig.8: Rotating with Ezrec the Waller Flag

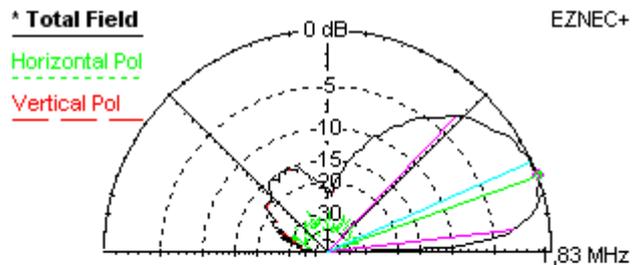
The Waller Flag compared to the original Flag.

Following are the snapshots of the Eznec patterns for both the Flags in the same IV3PRK environment, that is after detuning the nearby transmitting antenna.



^ Total Field		EZNEC+	
Horizontal Pol		Horizontal Pol	
Vertical Pol		Vertical Pol	
Elevation Plot			
Bearing	270,0 deg.	Cursor Elev	28,0 deg.
Outer Ring	-30,41 dBi	Gain	-30,41 dBi
			0,0 dBmax
			0,0 dBmax3D
3D Max Gain	-30,41 dBi		
Slice Max Gain	-30,41 dBi @ Elev Angle = 28,0 deg.		
Beamwidth	61,7 deg.; -3dB @ 7,9, 69,6 deg.		
Sidelobe Gain	-50,9 dBi @ Elev Angle = 166,0 deg.		
Front/Sidelobe	20,49 dB		

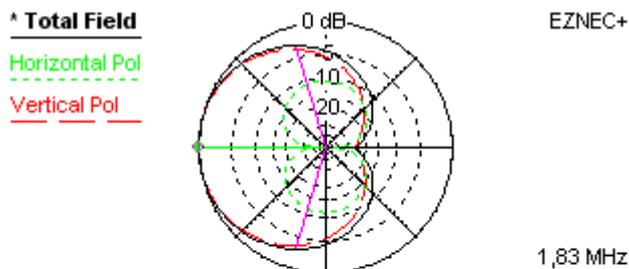
Fig.9: Original W7IUV Flag – Elev. plot



^ Total Field		EZNEC+	
Horizontal Pol		Horizontal Pol	
Vertical Pol		Vertical Pol	
Elevation Plot			
Bearing	272,0 deg.	Cursor Elev	20,0 deg.
Outer Ring	-55,46 dBi	Gain	-55,46 dBi
			0,0 dBmax
			0,0 dBmax3D
3D Max Gain	-55,46 dBi		
Slice Max Gain	-55,46 dBi @ Elev Angle = 20,0 deg.		
Beamwidth	39,6 deg.; -3dB @ 6,9, 46,5 deg.		
Sidelobe Gain	-55,53 dBi @ Elev Angle = 24,0 deg.		
Front/Sidelobe	0,07 dB		

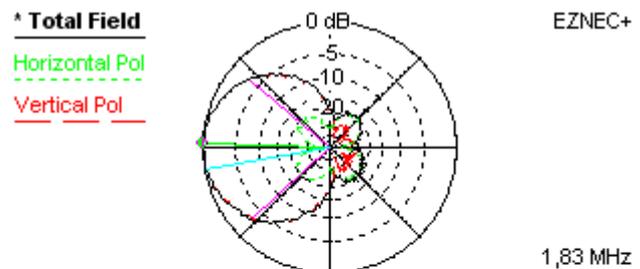
Fig.10: The Waller Flag – Elevation plot

The take-off angle is lower, and the lobe is much sharper in the Waller Flag, favouring the long-distance DX signals. In my personal situation, it should be a great benefit in reducing the Russian and eastern European QRM while working Far East and the Pacific in the same direction. Unfortunately, compared to the single Flag, there is that high angle back lobe, caused by the close spacing of the two loops, and almost impossible to reduce.



^ Total Field		EZNEC+	
Horizontal Pol		Horizontal Pol	
Vertical Pol		Vertical Pol	
Azimuth Plot			
Elevation Angle	28,0 deg.	Cursor Bear	270,0 deg.
Outer Ring	-30,41 dBi	Gain	-30,41 dBi
			0,0 dBmax
			0,0 dBmax3D
3D Max Gain	-30,41 dBi		
Slice Max Gain	-30,41 dBi @ Bearing = 270,0 deg.		
Front/Back	24,19 dB		
Beamwidth	147,5 deg.; -3dB @ 196,0, 343,5 deg.		
Sidelobe Gain	< -100 dBi		
Front/Sidelobe	> 100 dB		

Fig.11: Original W7IUV Flag – Azimuth plot



^ Total Field		EZNEC+	
Horizontal Pol		Horizontal Pol	
Vertical Pol		Vertical Pol	
Azimuth Plot			
Elevation Angle	20,0 deg.	Cursor Bear	272,0 deg.
Outer Ring	-55,46 dBi	Gain	-55,46 dBi
			0,0 dBmax
			0,0 dBmax3D
3D Max Gain	-55,46 dBi		
Slice Max Gain	-55,46 dBi @ Bearing = 272,0 deg.		
Front/Back	30,38 dB		
Beamwidth	82,9 deg.; -3dB @ 227,4, 310,3 deg.		
Sidelobe Gain	-55,56 dBi @ Bearing = 260,0 deg.		
Front/Sidelobe	0,1 dB		

Fig.12: The Waller Flag – Azimuth plot

The azimuth pattern of the Waller Flag is also very good, only 83 degrees of beamwidth, better than a typical four-square array but, as stated previously, there is a drawback which requires attention. The gain is 55 dB “negative”, thus 25 dB lower than on a single Flag, and we need two clean preamplifiers after being very careful with transformers to prevent noise entering the feedline.

The graphs on the right show the most meaning data of the two Flags taken every 30 degrees of rotation in the same environment.

The front to back ratio is a few dB's better for the original Flag in most of the bearing positions, hence meaningless.

Where we find a great marked advantage is in the RDF, the "Receiving Directivity Factor" with a stable difference of over 3.5 dB: awesome! RDF has lately become the most important and direct parameter used in ranking receiving antennas.

On www.w8ji.com, the Tom's site, we see that a 1.75 wl Beverage has an RDF of 11.16 dB.

The Waller Flag is above that, and can be rotated.

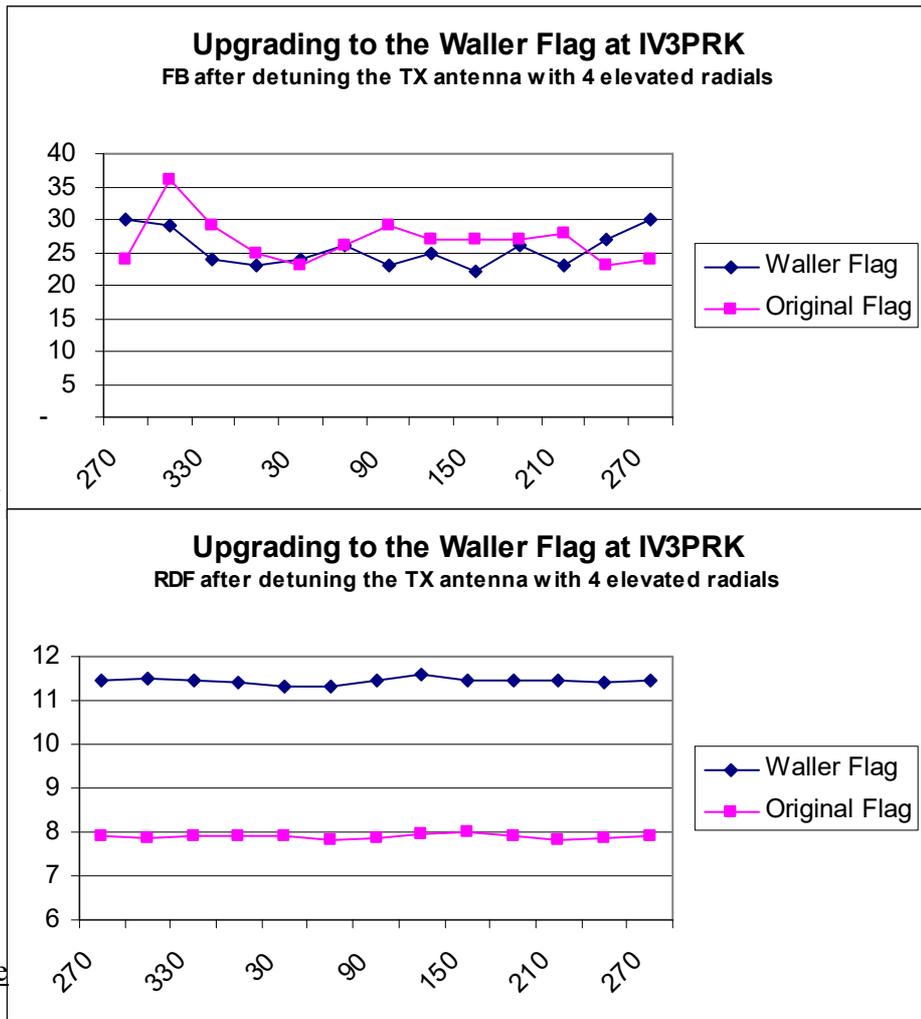


Fig.13: direct comparison between a single Flag and the Waller Flag

In the second part, I will cover the building of the "real" antenna and its tests "on the air" but, in the meantime, on www.n4is.com can be found all the designs and construction details of the "Waller Flag".

Let me thank again Doug Waller, NX4D, and Jose Carlos, N4IS, for the correspondence and sharing with me all their findings.

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Luis IV3PRK